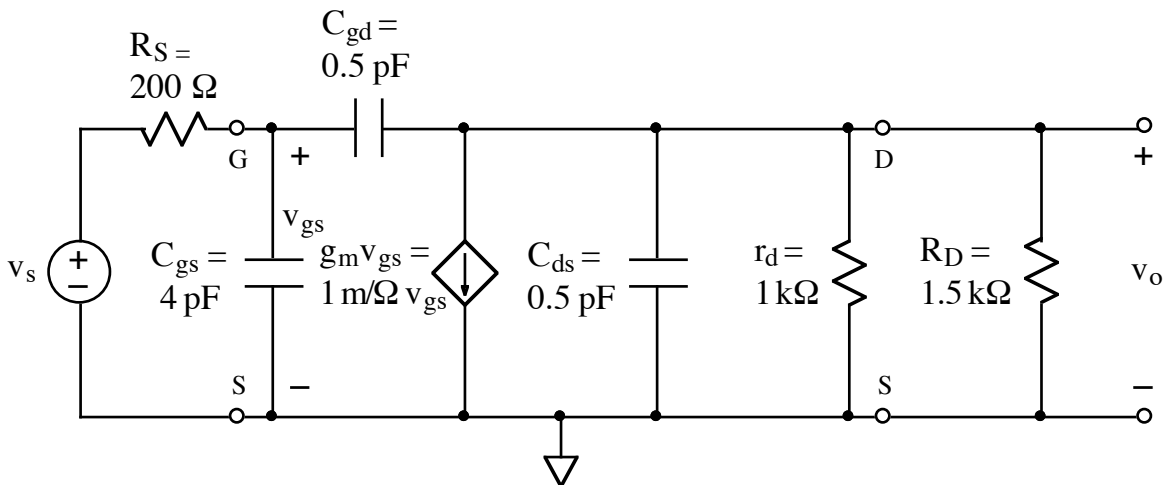
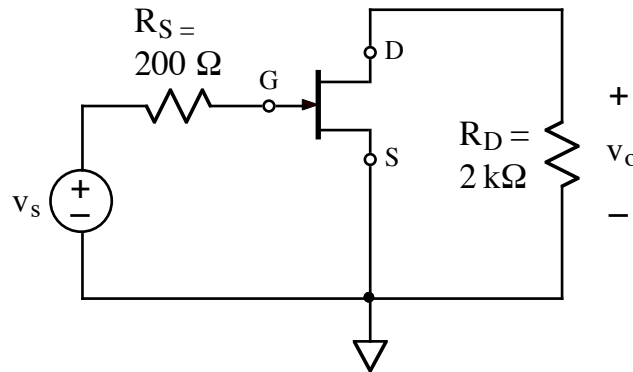


Ex:



$$v_s(t) = 2 \cos(10kt) \text{ V}$$

The above circuit diagrams show a common-source JFET amplifier and its high-frequency equivalent circuit. Find $v_o(t)$.

Sol'n: In this practical circuit, we have circuit values that allow us to make simplifying approximations.

We first calculate impedance values.

$$\omega = 10k \text{ r/s} \quad \text{from} \quad v_s(t) = 2 \cos(10kt) \text{ V}$$

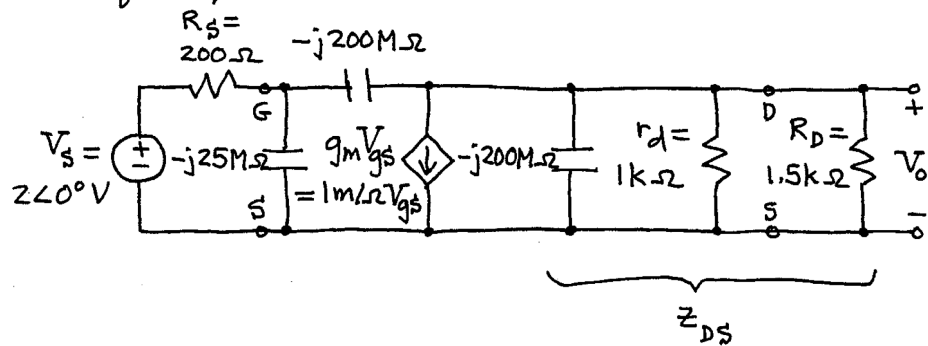
$$Z_{C_{gs}} = \frac{-j}{\omega C_{gs}} = \frac{-j \Omega}{10k \cdot 4p} = -j 25M \Omega$$

$$Z_{C_{gd}} = \frac{-j}{\omega C_{gd}} = \frac{-j}{10k \frac{1}{2} p} = -j 200M \Omega$$

$$Z_{C_{ds}} = \frac{-j}{\omega C_{ds}} = \frac{-j}{10k \frac{1}{2} p} = -j 200M \Omega$$

The phasor for $V_s(t)$ is $V_s = 2 \angle 0^\circ V$.

Frequency domain (or s-domain) model:



$$Z_{DS} = -j 200M \parallel 1k\Omega \parallel 1.5k\Omega$$

Starting with $1k\Omega \parallel 1.5k\Omega$ we have

$$1k\Omega \parallel 1.5k\Omega = 500\Omega \cdot 2 \parallel 3 = 500 \cdot \frac{6}{5}$$

$$= 600\Omega$$

$$\text{Thus, } Z_{DS} = -j 200M \parallel 600\Omega = \frac{1}{\frac{1}{600} - \frac{1}{j200M}}$$

Using $-\frac{1}{j} = j$ and rationalizing gives

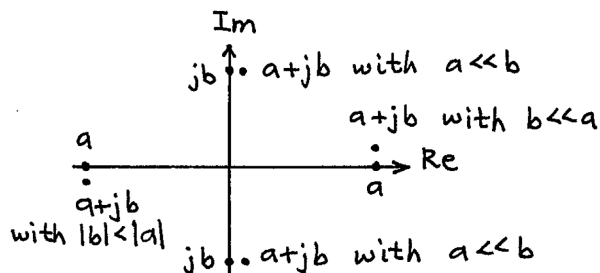
$$\begin{aligned}
 z_{DS} &= \frac{1}{\frac{1}{600} + \frac{j}{200M}} \frac{\frac{1}{600} - \frac{j}{200M}}{\frac{1}{600} - \frac{j}{200M}} \Omega \\
 &= \frac{\frac{1}{600} - \frac{j}{200M}}{\left(\frac{1}{600}\right)^2 + \left(\frac{1}{200M}\right)^2} \Omega \\
 &\approx \frac{\frac{1}{600} - \frac{j}{200M}}{\left(\frac{1}{600}\right)^2} \Omega \quad \text{Since } \frac{1}{200M} \ll \frac{1}{600} \\
 z_{DS} &\approx \frac{\frac{1}{600}}{\left(\frac{1}{600}\right)^2} \Omega = 600 \Omega
 \end{aligned}$$

In retrospect, we could have made the approximation that $-j200M \parallel 600 \Omega \approx 600 \Omega$.

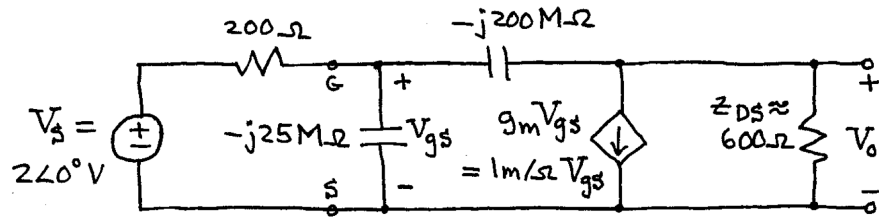
We may make this approximation despite the j in one of the quantities. In general, we may make the following approximations of complex values:

$$a + jb \approx a \quad \text{when } |b| \ll |a|$$

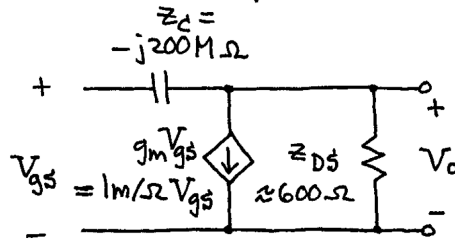
$$a + jb \approx jb \quad \text{when } |a| \ll |b|$$



With our z_{DS} value, we have a simplified model:



We now analyze the dependent source so we can replace it with an impedance, z_{eg} .



$$z_{eg} = \frac{V_o}{g_m V_{gs}} \quad \text{using Ohm's law to write } z_{eg} = V/I$$

Now we find a way to write V_o in terms of V_{gs} . We use a V -divider:

$$V_o = V_{gs} \frac{z_{eg} \parallel z_{DS}}{z_{eg} \parallel z_{DS} + z_c}$$

Substituting for V_o in our z_{eg} eq'n, we have

$$z_{eg} = \frac{V_{gs} \frac{z_{eg} \parallel z_{DS}}{z_{eg} \parallel z_{DS} + z_c}}{V_{gs} \cdot g_m}$$

$$z_{eg} = \frac{1}{g_m} \frac{\frac{z_{eg} z_{DS}}{z_{eg} + z_{DS}}}{\frac{z_{eg} z_{DS}}{z_{eg} + z_{DS}} + z_c}$$

$$z_{eg} = \frac{1}{g_m} \frac{z_{eg} z_{DS}}{z_{eg} z_{DS} + z_c (z_{eg} + z_{DS})}$$

Dividing top and bottom by z_{eg} gives the following:

$$z_{eg} = \frac{1}{g_m} \frac{z_{DS}}{z_{DS} + z_c + \frac{z_c z_{DS}}{z_{eg}}}$$

$$z_{eg} \left(z_{DS} + z_c + \frac{z_c z_{DS}}{z_{eg}} \right) = \frac{1}{g_m} z_{DS}$$

$$z_{eg} (z_{DS} + z_c) + z_c z_{DS} = \frac{1}{g_m} z_{DS}$$

$$z_{eg} \frac{(z_{DS} + z_c)}{z_{DS}} = \frac{1}{g_m} \frac{z_{DS} - z_c z_{DS}}{z_{DS}}$$

$$z_{eg} = \frac{1}{g_m} - z_c = \frac{1 \Omega - j200 \text{ M}\Omega}{1 \text{ m}} = \frac{1 - j200 \text{ M}\Omega}{1 + \frac{-j200 \text{ M}\Omega}{600 \Omega}}$$

$$z_{eg} = \frac{1 \text{ k} + j200 \text{ M} \Omega}{1 - j \frac{1}{3} \text{ M}}$$

The imaginary parts of the numerator and denominator are much larger than the real parts. Thus, we ignore the real parts.

$$z_{eg} \approx j200 \text{ M}\Omega / -j \frac{1}{3} \text{ M} \approx -600 \Omega$$

Now we have a problem: $z_{eg} \parallel z_{DS} = -\frac{600^2}{0} \Omega$.

That means $z_{eg} \parallel z_{DS} = \infty \Omega$.

It is a good idea to try a more exact calculation to be sure that $z_{eg} \parallel z_{DS}$ is much larger than $z_c = -j200M\Omega$.

We use conductance to simplify calculations.

$$\frac{1}{z_{eg} \parallel z_{DS}} = \frac{1}{z_{eg}} + \frac{1}{z_{DS}} = \frac{1 + \frac{z_c}{z_{DS}}}{\frac{1}{g_m} - z_c} + \frac{1}{z_{DS}}$$

$$= \frac{1}{z_{DS}} \left(\frac{z_{DS} + z_c}{\frac{1}{g_m} - z_c} + 1 \right)$$

$$= \frac{1}{z_{DS}} \left(\frac{z_{DS} + z_c}{\frac{1}{g_m} - z_c} + \frac{\frac{1}{g_m} - z_c}{\frac{1}{g_m} - z_c} \right)$$

$$= \frac{1}{z_{DS}} \left(\frac{z_{DS} + \frac{1}{g_m}}{\frac{1}{g_m} - z_c} \right)$$

$$= \frac{g_m + \frac{1}{z_{DS}}}{1 - g_m z_c}$$

$$= \frac{1m + \frac{1}{600}}{1 - 1m(-j200M)} \quad / \Omega$$

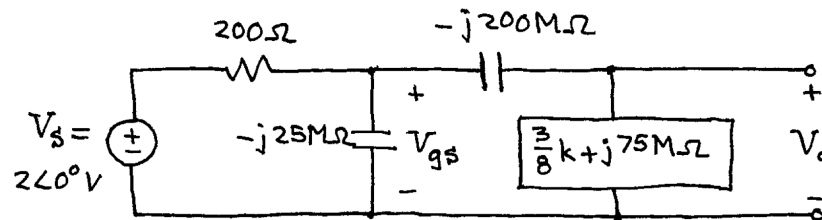
$$z_{eg} \parallel z_{DS} = \frac{1 + j200k}{\frac{1}{1k} + \frac{1}{600}} \Omega$$

$$z_{eg} \parallel z_{DS} = \frac{1 + j200k}{3 + 5} \Omega = \frac{3k(1 + j200k)}{8}$$

$$= \frac{3k + j75M\Omega}{8}$$

We see that the value is smaller than $z_c = -j200M\Omega$.

Our new, simplified model:



We use V-dividers to find V_o .

$$V_{gs} = V_s \cdot \frac{-j25M\Omega \parallel (-j200M + \overset{\text{small}}{\frac{3}{8}k + j75M\Omega})}{200 + -j25M\Omega \parallel (-j200M + \overset{\text{small}}{\frac{3}{8}k + j75M\Omega})}$$

$$V_{gs} \approx \frac{V_s \cdot (-j25M\Omega \parallel -j125M\Omega)}{200 - j25M\Omega \parallel -j125M\Omega}$$

where $-j25M\Omega \parallel -j125M\Omega = -j25M\Omega \cdot 1 \parallel 5$

$$= -j25M\Omega \cdot \frac{5}{6}$$

$$= -j \frac{125}{6} M\Omega$$

$$V_{gs} = \frac{V_s \cdot \left(-j \frac{125}{6} M\Omega\right)}{\overset{\text{small}}{200} - j \frac{125}{6} M\Omega} \approx V_s$$

$$V_o = V_{gs} \frac{\frac{3}{8} k + j 75 M\Omega}{\frac{3}{8} k + j 75 M\Omega - j 200 M\Omega}$$

$$V_o \approx V_{gs} \frac{j 75 M\Omega}{-j 125 M\Omega} = V_{gs} \left(-\frac{3}{5} \right)$$

$$V_o \approx 2 \angle 0^\circ V \left(-\frac{3}{5} \right) = -\frac{6}{5} \angle 0^\circ V = \frac{6}{5} \angle 180^\circ V$$

Note: a minus sign is the same as 180° of phase shift.

$$v_o(t) = \frac{6}{5} \cos(10kt + 180^\circ) V$$